



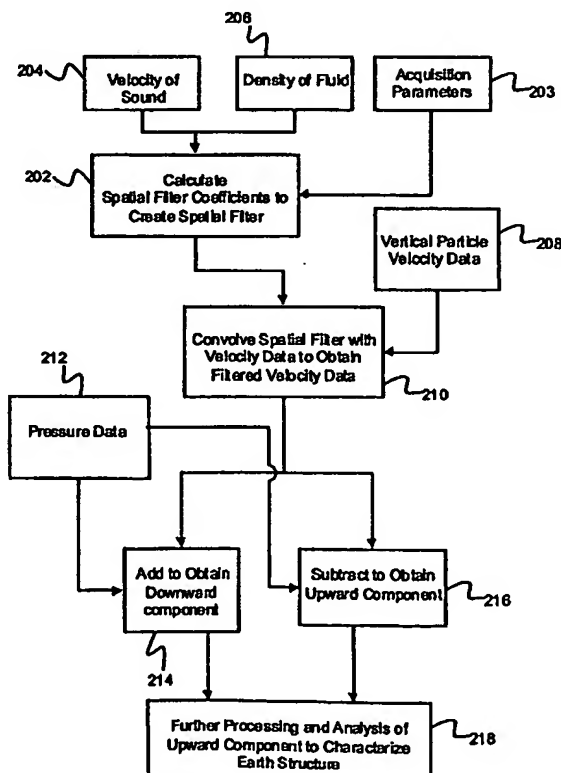
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁷ : G01V 1/36, 1/38		A1	(11) International Publication Number: WO 00/57207
			(43) International Publication Date: 28 September 2000 (28.09.00)
(21) International Application Number: PCT/GB00/01074		(74) Agent: WANG, William, L.; Intellectual Property Law Department, Schlumberger Cambridge Research Limited, High Cross, Maddingley Road, Cambridge CB3 0L (GB).	
(22) International Filing Date: 21 March 2000 (21.03.00)			
(30) Priority Data: 9906456.0 22 March 1999 (22.03.99) GB		(81) Designated States: AE, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CR, CU, CZ, DE, DK, DM, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).	
(71) Applicant (for all designated States except CA FR US): SCHLUMBERGER HOLDINGS LIMITED [-/-]; P.O. Box 71, Craigmuir Chambers, Road Town, Tortola (VG).			
(71) Applicant (for CA only): SCHLUMBERGER CANADA LIMITED [CA/CA]; Monenco Place, 24th floor, 801 6th Avenue, S.W., Calgary, Alberta T2P 3W2 (CA).			
(71) Applicant (for FR only): SERVICES PETROLIERS SCHLUMBERGER [FR/FR]; 42, rue Saint-Dominique, F-75007 Paris (FR).			
(72) Inventors; and (75) Inventors/Applicants (for US only): ROBERTSSON, Johan, Olof, Anders [SE/GB]; Stasjonsveien 28A, 0772 Oslo (NO). KRAUGH, Julian, Edward [GB/GB]; Sudbury Cottage, Cornish Hall End Road, Little Sampford, Essex CB10 2QS (GB). MARTIN, James, Edward [GB/NO]; Brenneveien 95, N-1349 Rykkinn (NO).		Published With international search report.	

(54) Title: METHOD AND SYSTEM FOR REDUCING EFFECTS OF SEA SURFACE GHOST CONTAMINATION IN SEISMIC DATA

(57) Abstract

An improved de-ghosting method and system that utilises multi-component marine seismic data recorded in a fluid medium is disclosed. The disclosed method makes use of two types of data: pressure data, that represents the pressure in the fluid medium, such as sea water, at a number of locations; and vertical particle motion data, that represents the vertical particle motion of the acoustic energy propagating in the fluid medium at a number of locations within the same spatial area as the pressure data. The vertical particle motion data can be in various forms, for example, velocity, pressure gradient, displacement, or acceleration. A spatial filter is designed so as to be effective at separating up and down propagating acoustic energy over substantially the entire range of non-horizontal incidence angles in the fluid medium. The spatial filter is applied to either the vertical particle motion data or to the pressure data, and then combined with the other data to generate pressure data that has its up and down propagating components separated.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece			TR	Turkey
BG	Bulgaria	HU	Hungary	ML	Mali	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MN	Mongolia	UA	Ukraine
BR	Brazil	IL	Israel	MR	Mauritania	UG	Uganda
BY	Belarus	IS	Iceland	MW	Malawi	US	United States of America
CA	Canada	IT	Italy	MX	Mexico	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NE	Niger	VN	Viet Nam
CG	Congo	KE	Kenya	NL	Netherlands	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NO	Norway	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	NZ	New Zealand		
CM	Cameroon			PL	Poland		
CN	China	KR	Republic of Korea	PT	Portugal		
CU	Cuba	KZ	Kazakhstan	RO	Romania		
CZ	Czech Republic	LC	Saint Lucia	RU	Russian Federation		
DE	Germany	LI	Liechtenstein	SD	Sudan		
DK	Denmark	LK	Sri Lanka	SE	Sweden		
EE	Estonia	LR	Liberia	SG	Singapore		

Method and System For Reducing Effects of Sea Surface Ghost
Contamination In Seismic Data

FIELD OF THE INVENTION:

5 The present invention relates to the field of
reducing the effects of sea-surface ghost reflections in
seismic data. In particular, the invention relates an
improved de-ghosting method that utilises measurements or
estimates of multi-component marine seismic data recorded in
10 a fluid medium.

BACKGROUND OF THE INVENTION:

Removing the ghost reflections from seismic data
is for many experimental configurations equivalent to
15 up/down wavefield separation of the recorded data. In such
configurations the down-going part of the wavefield
represents the ghost and the up-going wavefield represents
the desired signal. Exact filters for up/down separation of
multi-component wavefield measurements in Ocean Bottom Cable
20 (OBC) configurations have been derived by Amundsen and
Ikelle, and are described in U.K. Patent Application Number
9800741.2. An example of such a filter corresponding to de-
ghosting of pressure data at a frequency of 50 Hz for a
seafloor with P-velocity of 2000 m/s, S-velocity of 500 m/s
25 and density of 1800 kg/m³ is shown in Figure 2. At this
frequency, the maximum horizontal wavenumber for P-waves
right below the seafloor is $k=0.157 \text{ m}^{-1}$, whereas it is
 $k=0.628 \text{ m}^{-1}$ for S-waves. Notice the pole and the kink due to
a zero in the filter at these two wavenumbers, making
30 approximations necessary for robust filter implementations.
Figure 3 shows approximations to the filter. These filters

are only good at wavenumbers smaller than the wavenumber where the pole occurs. Hence, energy with low apparent velocities (for instance S-waves or Scholte waves at the seafloor) will not be treated properly. Moreover, since
5 they do not have a complex part, evanescent waves will also not be treated properly.

The OBC de-ghosting filters have been shown to work very well on synthetic data. However, apart from the difficulty with poles and zeros at critical wave numbers,
10 they also require knowledge about the properties of the immediate sub-bottom locations as well as hydrophone/geophone calibration and coupling compensation.

A normal incidence approximation to the de-ghosting filters for data acquired at the sea floor was
15 described by Barr, F.J. in U.S. Patent: 4,979,150, issued 1990, entitled 'System for attenuating water-column reflections', (hereinafter "Barr (1990)"). For all practical purposes, this was previously described by White, J.E., in a 1965 article entitled 'Seismic waves: radiation,
20 transmission and attenuation', McGraw-Hill (hereinafter "White (1965)"). However, this technique is not effective when the angle of incidence is away from vertical. Also, this technique does not completely correct for wide-angle scattering and the complex reflections from rough sea
25 surfaces. Additionally, it is believed that the OBC techniques described have not been used successfully in a fluid medium, such as with data gathered with towed streamers.

SUMMARY OF THE INVENTION:

Thus, it is an object of the present invention to provide a method of de-ghosting which improves attenuation of noise from substantially all non-horizontal angles of incidence.

It is an object of the present invention to provide a method of de-ghosting of seismic measurements made in a fluid medium which improves attenuation of the ghost as well as downward propagating noise from substantially all non-horizontal angles of incidence.

Also, it is an object of the present invention to provide a method of de-ghosting which is not critically dependent on knowledge about the properties of the surrounding fluid medium as well as hydrophone/geophone calibration and coupling compensation.

Also, it is an object of the present invention to provide a method of de-ghosting whose exact implementation is robust and can be implemented efficiently.

According to the invention, a method is described for sea surface ghost correction through the application of spatial filters to the case of marine seismic data acquired in a fluid medium. Using, for example, either typical towed streamer or vertical cable geometries. Preferably, both pressure and vertical velocity measurements are acquired along the streamer. The invention takes advantage of non-conventional velocity measurements taken along a marine towed streamer, for example. New streamer designs are currently under development and are expected to become commercially available in the near future. For example, the Defence Evaluation and Research Agency (DERA), based in

Dorset, U.K., claim to have successfully built such a streamer for high frequency sonar applications.

According to an alternative embodiment, the invention is also applicable to seismic data obtained with configurations of multiple conventional streamers. Here, the filters make use of vertical pressure gradient measurements, as opposed to velocity measurements. According to the invention, an estimate of the vertical pressure gradient can be obtained from over/under twin streamer data, or more generally from streamer data acquired by a plurality of streamers where the streamers are spatially deployed in a manner analogous to that described in U.K Patent Application Number 9820049.6, by Robertsson, entitled 'Seismic detection apparatus and related method' filed in 1998 (hereinafter "Robertsson (1998)"). For example, three streamers can be used, forming a triangular shape cross-section along their length. Vertical pressure gradient data can also be obtained from pressure gradient measuring devices.

According to the invention, the filters fully account for the rough sea perturbed ghost, showing improvement over other techniques based on normal incidence approximations (see e.g., White (1965)), which have been applied to data recorded at the sea floor.

Advantageously, according to preferred embodiments of the invention, the results are not sensitive to streamer depth, allowing the streamer(s) to be towed at depths below swell noise contamination, hence opening up the acquisition weather window where shallow towed streamer data would be unusable. Local streamer accelerations will be minimised in the deep water flow regime, improving resolution of the

pressure, multi-component velocity and pressure gradient measurements.

Advantageously, according to preferred embodiments of the invention, there are no filter poles in the data
5 window, except for seismic energy propagating horizontally at the compressional wave speed in water.

Advantageously, according to preferred embodiments of the invention, the filter is not critically dependent on detailed knowledge of the physical properties of the
10 surrounding fluid medium.

The filters can be simple spatial convolutions, and with the regular geometry of typical towed streamer acquisition the filters are efficient to apply in the frequency-wavenumber (FK) domain. The filters can also be
15 formulated for application in other domains, such as time-space and intercept time-slowness (τ -p).

According to the invention, a method of reducing the effects in seismic data of downward propagating reflected and scattered acoustic energy travelling in a
20 fluid medium is provided. The method advantageously makes use of two types of data: pressure data, that represents the pressure in the fluid medium, such as sea water, at a number of locations; and vertical particle motion data, that represents the vertical particle motion of the acoustic
25 energy propagating in the fluid medium at a number of locations within the same spatial area as the pressure data. The distance between the locations that are represented by the pressure data and the vertical particle motion data in each case is preferably less than the Nyquist spatial
30 sampling criterion. The vertical particle motion data can

be in various forms, for example, velocity, pressure gradient, displacement, or acceleration.

The spatial filter is created by calculating a number of coefficients that are based on the velocity of
5 sound in the fluid medium and the density of the fluid medium. The spatial filter is designed so as to be effective at separating up and down propagating acoustic energy over substantially the entire range of non-horizontal incidence angles in the fluid medium.

10 The spatial filter is applied to either the vertical particle motion data or to the pressure data, and then combined with the other data to generate pressure data that has its up and down propagating components separated. The separated data are then processed further and analysed.
15 Ordinarily the down-going data would be analysed, but the up going data could be used instead if the sea surface was sufficiently calm.

According to an alternative embodiment, a method of reducing the effects of downward propagating reflected
20 and scattered acoustic energy travelling in a fluid medium is provided wherein the pressure data and vertical particle motion data represent variations caused by a first source event and a second source event. The source events are preferably generated by firing a seismic source at different
25 locations at different times, and the distance between the locations is preferably less than the Nyquist spatial sampling criterion.

The present invention is also embodied in a computer-readable medium which can be used for directing an
30 apparatus, preferably a computer, to reduce the effects in seismic data of downward propagating reflected and scattered

acoustic energy travelling in a fluid medium as otherwise described herein.

BRIEF DESCRIPTION OF THE DRAWINGS:

5 Figure 1 shows examples of simple seismic ray paths for primary events, and ghosts that are last reflected from the rough sea-surface;

 Figure 2 shows an exact pressure de-ghosting filter for OBC data for a seafloor with P-velocity of 2000
10 m/s, S-velocity of 500 m/s and density of 1800 kg/m³; the upper panel shows the Real part of exact filter; and the lower panel shows the Imaginary part of exact filter;

 Figure 3 shows the Real part of the exact OBC de-ghosting filter (in the solid line) shown in Figure 2, the
15 first order Taylor approximation filter (in the plus line), and the first four fractional expansion approximations filters (in the dash-dotted lines);

 Figure 4 illustrates the potential impact of 3D rough sea surface ghost reflection and scattering on
20 consistency of the seismic data waveform;

 Figure 5 illustrates the potential impact of the rough sea surface ghost perturbation on time-lapse seismic data quality;

 Figures 6a-6f show various embodiments for data
25 acquisition set-ups and streamer configurations according to preferred embodiments of the invention;

 Figure 7 shows an exemplary two-dimensional spatial filter response (ω/k_z) for $dx=6m$;

 Figure 8 is a flow chart illustrating some of the
30 steps of the de-ghosting method for the combination of

pressure and vertical velocity data to achieve separated pressure data, according to a preferred embodiment of the invention;

Figure 9 schematically illustrates an example of a data processor that can be used to carry out preferred embodiments of the invention;

Figure 10 shows an example of a shot record computed below a 4m significant wave height (SWH) rough sea surface, the left panel shows pressure, and the right panel shows vertical velocity scaled by water density and the compressional wave speed in water;

Figure 11 illustrates de-ghosting results of the shot record in Figure 10, the left panel shows results using the vertical incidence approximation, and the right panel illustrates the exact solution;

Figure 12 illustrates an example of de-ghosting results in detail for a single trace at 330m offset corresponding to an arrival angle of about 37 degrees, the upper panel shows the vertical incidence approximation, and the lower panel shows the Exact solution; and

Figures 13a-b illustrate two possible examples of multi-component streamer design.

25 DETAILED DESCRIPTION OF THE INVENTION:

Figure 1 is a schematic diagram showing reflections between a sea surface (S), sea floor (W) and a target reflector (T). Various events that will be recorded in the seismogram are shown and are labelled according to the series of interfaces they are reflected at. The stars

indicate the seismic source and the arrowheads indicate the direction of propagation at the receiver. Events ending with 'S' were last reflected at the rough sea surface and are called receiver ghost events. Down-going sea-surface
5 ghost reflections are an undesirable source of contamination, obscuring the interpretation of the desired up-going reflections from the earth's sub-surface.

Rough seas are a source of noise in seismic data. Aside from the often-observed swell noise, further errors
10 are introduced into the reflection events by ghost reflection and scattering from the rough sea surface. The rough sea perturbed ghost events introduce errors that are significant for time-lapse seismic surveying and the reliable acquisition of repeatable data for stratigraphic
15 inversion.

The effect of the rough sea is to perturb the amplitude and arrival time of the sea surface reflection ghost and add a scattering coda, or tail, to the ghost impulse. The impulse response can be calculated by finite
20 difference or Kirchhoff methods (for example) from a scattering surface which represents statistically typical rough sea surfaces. For example, a directional form of the Pierson-Moskowitz spectrum described by Pierson, W.J. and Moskowitz, L., 1964 'A proposed Spectral Form for Fully
25 Developed Wind Seas Based on the Similarity Theory of S. A. Kitaigorodskii' J. Geo. Res., 69, 24, 5181-5190, (hereinafter "Pierson and Moskowitz (1964)"), and Hasselmann, D. E., Dunckel, M. and Ewing, J.A., 1980 'Directional Wave Spectra Observed During JONSWAP 1973', J.
30 Phys. Oceanography, v10, 1264-1280, (hereinafter "Hasselmann et al, (1980)"). Both the wind's speed and direction define

the spectra. The Significant Wave Height ("SWH") is the subjective peak to trough wave amplitude, and is about equal to 4 times the RMS wave height. Different realisations are obtained by multiplying the 2D surface spectrum by Gaussian random complex numbers.

Figure 4 shows an example of rough sea impulses along a 400m 2D line (e.g. streamer) computed under a 2m SWH 3D rough sea surface. The streamer shape affects the details of the impulses, and in this example the streamer is straight and horizontal. Figure 4 shows, from top to bottom: The ghost wavelet (white trough) arrival time, the ghost wavelet maximum amplitude, a section through the rough sea realisation above the streamer, and the computed rough sea impulses. The black peak is the upward travelling wave, which is unperturbed; the white trough is the sea ghost reflected from the rough sea surface. The latter part of the wavelet at each receiver is the scattering coda from increasingly more distant parts of the surface. Notice that the amplitude and arrival time ghost perturbations change fairly slowly with offset. The arrival time perturbations are governed by the dominant wavelengths in the sea surface, which are 100-200m for 2-4m SWH seas, and the amplitude perturbations are governed by the curvature of the sea surface which has an RMS radius of about 80m and is fairly independent of sea state. The diffraction coda appear as quasi-random noise following the ghost pulse.

The rough sea perturbations cause a partial fill and a shift of the ghost notch in the frequency domain. They also add a small ripple to the spectrum, which amounts to 1-2dB of error for typical sea states. In the post stack

domain this translates to an error in the signal that is about -20dB for a 2m SWH sea.

Figure 5 shows an example of how such an error can be significant for time-lapse surveys. The panel on the top left shows a post-stack time-migrated synthetic finite difference seismic section. The top middle panel shows the same data but after simulating production in the oil reservoir by shifting the oil water contact by 6m and introducing a 6m partial depletion zone above this. The small difference is just noticeable on the black leg of the reflection to the right of the fault just below 2s two-way travel-time. The panel on the right (top) shows the difference between these two sections multiplied by a factor of 10. This is the ideal seismic response from the time-lapse anomaly.

The left and middle bottom panels show the same seismic sections, but rough sea perturbations for a 2m SWH (as described above) have been added to the raw data before processing. Note that different rough sea effects are added to each model to represent the different seas at the time of acquisition. The difference obtained between the two sections is shown on the bottom right panel (again multiplied by a factor of 10). The errors in the reflector amplitude and phase (caused by the rough sea perturbations) introduce noise of similar amplitude to the true seismic time-lapse response. To a great extent, the true response is masked by these rough sea perturbations. A method for correcting these types of error is clearly important in such a case, and with the increasing requirement for higher quality, low noise-floor data, correction for the rough sea ghost becomes necessary even in modest sea states.

Equation (1) gives the frequency domain expression for a preferred filter relating the up-going pressure field, $p^u(x)$, to the total pressure, $p(x)$, and vertical particle velocity, $v_z(x)$.

5

$$p^u(x) = 0.5 \left[p(x) + \frac{\rho\omega}{k_z} * v_z(x) \right] \quad (1)$$

10

where k_z is the vertical wavenumber for compressional waves in the water, ρ is the density of water and $*$ denotes spatial convolution.

The vertical wavenumber is calculated from $k_z^2 = k^2 - k_x^2$ for two-dimensional survey geometries, or $k_z^2 = k^2 - k_x^2 - k_y^2$ for three-dimensional survey geometries, with $k^2 = \omega^2/c^2$, where c is the compressional wave speed in the water and k_x is the horizontal wavenumber for compressional waves in the water. The regular sampling of typical towed streamer data allows k_z to be calculated efficiently in the FK domain. Figure 7 shows an example of the filter response, ω/k_z for $dx=6m$ (the filter is normalised for the display to an arbitrary value). Infinite gain poles occur when k_z is zero. This corresponds to energy propagating horizontally (at the compressional wave speed in water). For towed streamer data, there is little signal energy with this apparent velocity, any noise present in the data with this apparent velocity should be filtered out prior to the filter application, or, the filter should be tapered at the poles prior to application to avoid amplification of the noise.

The traditional filter (White (1965), Barr, (1990)) is equation (2):

$$p'' = 0.5[p + \rho c v_z] \quad (2)$$

5

By comparison to equation (1), we see that this is a normal incidence approximation, which occurs when k_x is zero. This is implemented as a simple scaling of the vertical velocity trace followed by its addition to the pressure trace.

10

Equation (1) can also be formulated in terms of the vertical pressure gradient ($dp(x)/dz$). The vertical pressure gradient is proportional to the vertical acceleration:

15

$$dp(x)/dz = \rho dv_z(x)/dt \quad (3)$$

Integrating in the frequency domain through division of $i\omega$, and substituting in equation (1) gives:

20

$$p''(x) = 0.5 \left[p(x) + \frac{1}{ik_z} * dp(x)/dz \right] \quad (4)$$

Figures 6a-6f show various embodiments for data acquisition set-ups and streamer configurations according to preferred embodiments of the invention. Figure 6a shows a seismic vessel 120 towing a seismic source 110 and a seismic streamer 118. The sea surface is shown by reference number 112. In this example, the depth of streamer 118 is about 60 meters, however those of skill in the art will recognise

30

that a much shallower depth would ordinarily be used such as 6-10 meters. The dashed arrows 122a-d show paths of seismic energy from source 110. Arrow 122a shows the initial down-going seismic energy. Arrow 122b shows a portion of the seismic energy that is transmitted through the sea floor 114. Arrow 122c shows an up-going reflection. Arrow 122d shows a down-going ghost reflected from the surface. According to the invention, the down-going rough sea receiver ghost 122d can be removed from the seismic data.

Figures 6b-6f show greater detail of acquisition set-ups and streamer configurations, according to the invention. Figure 6b shows a multi-component streamer 124. The streamer 124 comprises multiple hydrophones (measuring pressure) 126a, 126b, and 126c, and multiple 3C geophones (measuring particle velocity in three directions x, y, and z) 128a, 128b, and 128c. The spacing between the hydrophones 126a and 126b, and between geophones 128a and 128b is shown to be less than 12 meters. Additionally, the preferred spacing in relation to the frequencies of interest is discussed in greater detail below.

Figure 6c shows a streamer 130 that comprises multiple hydrophones 132a, 132b, and 132c, and multiple pressure gradient measuring devices 134a, 134b, and 134c. The spacing between the hydrophones 132a and 132b, and between pressure gradient measuring devices 134a and 134b is shown to be less than 12 meters.

Figure 6d shows a multi-streamer configuration that comprises hydrophone streamers 140a and 140b. The streamers comprise multiple hydrophones 142a, 142b, and 142c in the case of streamer 140a, and 142d, 142e, and 142f in the case of streamer 140b. The spacing between the

hydrophones is shown to be less than 12 meters. The separation between streamers 140a and 140b in the example shown in Figure 6d is less than 2 meters. Although the preferred separation is less than 2 meters, greater
5 separations are contemplated as being within the scope of the invention. Figure 6e shows a cross sectional view of a dual streamer arrangement. Figure 6f shows a multi-streamer configuration comprising three hydrophone streamers 140a, 140b, and 140c.

10 Adequate spatial sampling of the wavefield is highly preferred for the successful application of the de-ghosting filters. For typical towed streamer marine data, a spatial sampling interval of 12m is adequate for all incidence angles. However, to accurately spatially sample
15 all frequencies up to 125Hz (for all incidence angles), a spatial sampling interval of 6.25 meters is preferred. These spacings are determined according to the Nyquist spatial sampling criterion. Note that if all incidence angles are not required, a coarser spacing than described
20 above can be used. The filters can be applied equally to both group formed or point receiver data.

Figure 8 is a flow chart illustrating some of the steps of the de-ghosting method for the combination of pressure and vertical velocity data to achieve separated
25 pressure data, according to a preferred embodiment of the invention. In step 202, spatial filter coefficients are calculated. The coefficients are preferably dependent on the characteristics of the acquisition parameters 203 (such as the temporal sample interval of the pressure and particle
30 motion data, the spatial separation of the vertical particle motion measuring devices, and the spatial aperture of the

filter), the density of the fluid medium 206, and the speed of the compressional wave in the fluid medium (or velocity of sound) 204. Vertical particle motion data 208 and pressure data 212 are received, typically stored as time domain traces on a magnetic tape or disk. In step 210, the vertical particle motion data 208 are convolved in with the spatial filter to yield filtered vertical particle motion data. In step 214 the filtered vertical particle motion data are added to pressure data 212 to give the downward propagating component of the separated pressure data. Alternatively, in step 216 the filtered vertical particle motion data are subtracted from pressure data 212 to give the upward propagating component of the separated pressure data. Finally, in step 218 the upward component is further processes and analysed.

processor
The processing described herein is preferably performed on a data processor configured to process large amounts of data. For example, Figure 9 illustrates one possible configuration for such a data processor. The data processor typically consists of one or more central processing units 350, main memory 352, communications or I/O modules 354, graphics devices 356, a floating point accelerator 358, and mass storage devices such as tapes and discs 360. It will be understood by those skilled in the art that tapes and discs 360 are computer-readable media that can contain programs used to direct the data processor to carry out the processing described herein.

Figure 10 shows a shot record example, computed under a 4m Significant Wave Height (SWH) sea and using the finite-difference method described by Robertsson, J.O.A., Blanch, J.O. and Symes, W.W., 1994 'Viscoelastic finite-

difference modelling' *Geophysics*, 59, 1444-1456 (hereinafter "Robertsson et al. (1994)") and Robertsson, J.O.A., 1996 'A Numerical Free-Surface Condition for Elastic/Viscoelastic Finite-difference modelling in the Presence of Topography', *Geophysics*, 61, 6, 1921-1934 (hereinafter "Robertsson (1996)"). The streamer depth in this example is 60m. The left panel shows the pressure response and the right panel shows the vertical velocity response scaled by the water density and the compressional wave speed in water. A point source 50Hz Ricker wavelet was used and the streamer depth was 60m in this example. The choice of streamer depth allows a clear separation of the downward travelling ghost from the upward travelling reflection energy for visual clarity of the de-ghosting results. The trace spacing on the plot is 24m. A single reflection and its associated ghost are shown, along with the direct wave travelling in the water layer. Perturbations in the ghost wavelet and scattering noise from the rough sea surface are evident.

Figure 11 shows the results of de-ghosting the shot record shown in Figure 10. The left panel shows the result using the normal incidence approximation and the right panel shows the result using the exact solution. The exact solution shows a consistent response over all offsets, whereas the normal incidence approximation starts to break down at incident angles greater than about 20 degrees, and shows a poorer result at the near offsets. Note that the direct wave is not amplified by the exact filter application even though the poles of the filter lie close to its apparent velocity. The exact filter is tapered before application such that it has near unity response for frequencies and wavenumbers corresponding to apparent

velocities of 1500m/s and greater. The weak event just below the signal reflection is a reflection from the side absorbing boundary of the model. It is upward travelling and hence untouched by the filter.

5 Figure 12 shows details of the de-ghosted results for a single trace from Figure 11. The trace offset is 330m corresponding to a 37 degree incidence angle. The upper panel shows the normal incidence approximation, and the lower panel shows the exact solution. Not only does the
10 exact solution provide a superior result in terms of the de-ghosting, but also in terms of amplitude preservation of the signal reflection - the upper panel shows loss of signal amplitude after the de-ghosting.

 The filters described herein are applicable to,
15 for example, measurements of both pressure and vertical velocity along the streamer. Currently, however, only pressure measurements are commercially available. Therefore, engineering of streamer sections that are capable of commercially measuring vertical velocity is preferred in
20 order to implement the filters.

 Figures 13a-b illustrate two possible examples of multi-component streamer design. Figure 13a shows a coincident pressure and single 3-component geophone. In this design, the 3-component geophone is perfectly decoupled
25 from the streamer. Figure 13b shows a coincident pressure and twin 3-component geophones. In this design, one of the 3-component geophones is decoupled from the streamer, the other is coupled to the streamer; measurements from both are combined to remove streamer motion from the data.

30 In an alternative formulation, the filters make use of vertical pressure gradient measurements. An estimate

of vertical pressure gradient can be obtained from over/under twin streamers (such as shown in Figures 6d and 6e) and multiple streamers (such as shown in Figure 6f) deployed in configurations analogous to that described in Robertsson (1998), allowing the filters to be directly applied to such data. However, for the results to remain sufficiently accurate, the streamers should not be vertically separated by more than 2m for seismic frequencies below approximately 80Hz.

10 An important advantage of multiple streamer configurations such as shown in Figure 6f is that their relative locations are less crucial than for over/under twin streamer geometries, where the two streamers are preferably directly above one another.

15 The filters described here are applied in 2D (along the streamer) to data modelled in 2D. The application to towed streamer configurations naturally lends itself to this implementation, the cross-line (streamer) sampling of the wavefield being usually insufficient for a full 3D implementation. Application of these filters to real data (with ghost reflections from 3D sea surfaces) will give rise to residual errors caused by scattering of the wavefield from the cross-line direction. This error increases with frequency though is less than 0.5dB in amplitude and 3.6° in phase for frequencies up to 150Hz, for a 4m SWH sea. These small residual noise levels are acceptable when time-lapse seismic surveys are to be conducted.

25 Invoking the principle of reciprocity, the filters can be applied in the common receiver domain to remove the downward travelling source ghost. Reciprocity simply means
30

that the locations of source and receiver pairs can be
interchanged, (the ray path remaining the same) without
altering the seismic response. Figure 1 can also be used to
define the source ghost if the stars are now regarded as
5 receivers and the direction of the arrows is reversed, with
the source now being located at the arrow. This application
is particularly relevant for data acquired using vertical
cables, which may be tethered, for example, to the sea
floor, or suspended from buoys. In the case of Figure 6a,
10 those of skill in the art will understand that as the
seismic vessel 120 travels through the water, the firing
position of source 110 will change. The different positions
of source 110 can be then be used to construct data in the
common receiver domain as is well known in the art.

15 While preferred embodiments of the invention have
been described, the descriptions and figures are merely
illustrative and are not intended to limit the present
invention.

CLAIMS

What is claimed is:

- 5 1. A method of reducing the effects in seismic data of downward propagating reflected and scattered acoustic energy travelling in a fluid medium comprising the steps of:
- 10 receiving pressure data representing at least the pressure in the fluid medium at a first location and a second location, the first location being in close proximity to the second location;
- 15 receiving vertical particle motion data representing at least the vertical particle motion of acoustic energy propagating in the fluid medium at a third location and a fourth location, the third location being in close proximity to the fourth location, and the first, second, third and fourth locations being within a spatial area;
- 20 calculating a plurality of spatial filter coefficients based in part on the velocity of sound in the fluid medium, the density of the fluid medium and a plurality of acquisition parameters, thereby creating a spatial filter which is designed so as to be effective
- 25 at separating up and down propagating acoustic energy over a range of non-vertical incidence angles in the fluid medium;
- 30 applying the spatial filter to the vertical particle motion data to generate filtered particle motion data;

combining the filtered particle motion data with the pressure data to generate separated pressure data, the separated pressure data having up and down propagating components separated; and

5 analysing at least part of the up or down propagating component of the separated pressure data.

2. The method of claim 1 wherein the acquisition parameters include the temporal sampling interval, the
10 spatial sampling interval, and the number of independent locations at which the pressure and vertical particle motion data are measured.

3. The method of claim 1 wherein the vertical
15 particle motion data is measured using one or more multi-component streamers.

4. The method of claim 1 wherein the vertical particle motion of the acoustic energy represented in said
20 vertical particle motion data is the particle velocity of the acoustic energy.

5. The method of claim 1 wherein the vertical particle motion of the acoustic energy represented in said
25 vertical particle motion data is the vertical pressure gradient of the acoustic energy.

6. The method of claim 5 wherein the pressure gradient is measured using at least two parallel streamer
30 cables in close proximity and vertically offset from one another.

7. The method of claim 1 wherein the vertical particle motion of the acoustic energy represented in said vertical particle motion data is the vertical displacement
5 of the acoustic energy.

8. The method of claim 1 wherein the vertical particle motion of the acoustic energy represented in said vertical particle motion data is the vertical acceleration
10 of the acoustic energy.

9. The method of claim 1 wherein the distance between the first location and the second location and the distance between the third location and the fourth location
15 is less than the Nyquist spatial sampling criterion.

10. The method of claim 9 wherein the spatial area is substantially a portion of a line, and the range of non-vertical incidence angles includes substantially all
20 non-horizontal incidence angles within a vertical plane that passes through the portion of line.

11. The method of claim 9 wherein the spatial area is a portion of a substantially planar region, and the
25 range of non-vertical incidence angles include substantially all non-horizontal incidence angles.

12. A method of reducing the effects in seismic
30 data of downward propagating reflected and scattered

acoustic energy travelling in a fluid medium comprising the steps of:

5 receiving pressure data representing at least the pressure in the fluid medium at a first location and a second location, the first location being in close proximity to the second location;

10 receiving vertical particle motion data representing at least the vertical particle motion of acoustic energy propagating in the fluid medium at a third location and a fourth location, the third location being in close proximity to the fourth location, and the first, second, third and fourth locations being within a spatial area;

15 calculating a plurality of spatial filter coefficients based in part on the velocity of sound in the fluid medium and the density of the fluid medium, thereby creating a spatial filter which is designed so as to be effective at separating up and down propagating acoustic energy over a range of non-

20 horizontal incidence angles in the fluid medium;

 applying the spatial filter to the pressure data to generate filtered pressure data;

25 combining the filtered pressure data with the vertical particle motion data to generate separated pressure data, the separated pressure data having up and down propagating components separated; and

 analysing at least part of the up or down propagating component of the separated pressure data.

30

13. The method of claim 12 wherein the distance between the first location and the second location and the distance between the third location and the fourth location is less than the Nyquist spatial sampling criterion.

5

14. The method of claim 12 wherein the vertical particle motion data is measured using one or more multi-component streamers.

10

15. The method of claim 12 wherein the vertical particle motion of the acoustic energy represented in said vertical particle motion data is the particle velocity of the acoustic energy.

15

16. The method of claim 12 wherein the vertical particle motion of the acoustic energy represented in said vertical particle motion data is the vertical pressure gradient of the acoustic energy.

20

17. The method of claim 16 wherein the pressure gradient is measured using at least two parallel streamer cables in close proximity and vertically offset from one another.

25

18. A method of reducing the effects in seismic data of downward propagating reflected and scattered acoustic energy travelling in a fluid medium comprising the steps of:

30

receiving pressure data representing at least variations in pressure in the fluid medium at a first location, the variations caused in part by a first

source event and a second source event, the first source event and the second source event being within a spatial area;

5 receiving vertical particle motion data representing at least the vertical particle motion of acoustic energy propagating in the fluid medium at a second location, the acoustic energy being caused in part by the first source event and the second source event;

10 calculating a plurality of spatial filter coefficients based in part on the velocity of sound in the fluid medium and the density of the fluid medium, thereby creating a spatial filter which is designed so as to be effective at separating up and down
15 propagating acoustic energy from the first source event and second source event over a range of non-horizontal incidence angles in the fluid medium;

 applying the spatial filter to the vertical particle motion data to generate filtered particle
20 motion data;

 combining the filtered particle motion data with the pressure data to generate separated pressure data, the separated pressure data having up and down propagating components separated; and

25 analysing at least part of the up or down propagating component of the separated pressure data.

19. The method of claim 18 wherein the first source event and the second source event are generated by
30 firing a seismic source at different locations at different times, and the distance between the location of the first

source event and the location of the second source event is less than the Nyquist spatial sampling criterion.

20. The method of claim 18 wherein the vertical
5 particle motion data is measured using one or more multi-component streamers.

21. The method of claim 18 wherein the vertical
particle motion of the acoustic energy represented in said
10 vertical particle motion data is the particle velocity of the acoustic energy.

22. The method of claim 18 wherein the vertical
particle motion of the acoustic energy represented in said
15 vertical particle motion data is the vertical pressure gradient of the acoustic energy.

23. The method of claim 22 wherein the pressure
gradient is measured using at least two parallel streamer
20 cables in close proximity and vertically offset from one another.

24. A computer-readable medium which can be used
for directing an apparatus to reduce the effects in seismic
25 data of downward propagating reflected and scattered acoustic energy travelling in a fluid medium comprising:

means for retrieving pressure data
representing at least the pressure in the fluid medium
at a first location and a second location, the first
30 location being in close proximity to the second location;

means for retrieving vertical particle motion data representing at least the vertical particle motion of acoustic energy propagating in the fluid medium at a third location and a fourth location, the third location being in close proximity to the fourth location, and the first, second, third and fourth locations being within a spatial area;

means for calculating a plurality of spatial filter coefficients based in part on the velocity of sound in the fluid medium, the density of the fluid medium and a plurality of acquisition parameters, thereby creating a spatial filter which is designed so as to be effective at separating up and down propagating acoustic energy over a range of non-vertical incidence angles in the fluid medium;

means for applying the spatial filter to the vertical particle motion data to generate filtered particle motion data;

means for combining the filtered particle motion data with the pressure data to generate separated pressure data, the separated pressure data having up and down propagating components separated; and

means for analysing at least part of the up or down propagating component of the separated pressure data.

25. The computer-readable medium of claim 24 wherein the distance between the first location and the second location and the distance between the third location

and the fourth location is less than the Nyquist spatial sampling criterion.

26. The computer-readable medium of claim 24
5 wherein the vertical particle motion data is measured using one or more multi-component streamers.

27. The computer-readable medium of claim 24
wherein the vertical particle motion of the acoustic energy
10 represented in said vertical particle motion data is the particle velocity of the acoustic energy.

28. The computer-readable medium of claim 24
wherein the vertical particle motion of the acoustic energy
15 represented in said vertical particle motion data is the vertical pressure gradient of the acoustic energy.

29. The computer-readable medium of claim 28
wherein the pressure gradient is measured using at least two
20 parallel streamer cables in close proximity and vertically offset from one another.

1/13

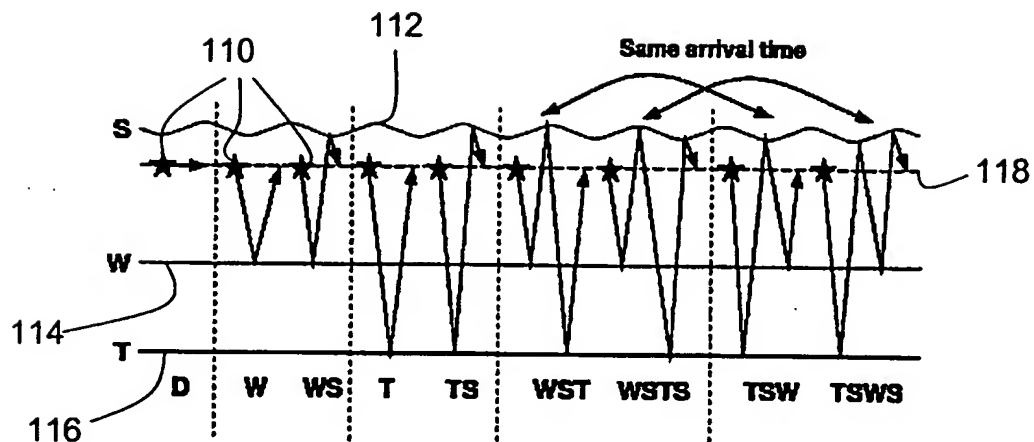


Figure 1

2/13

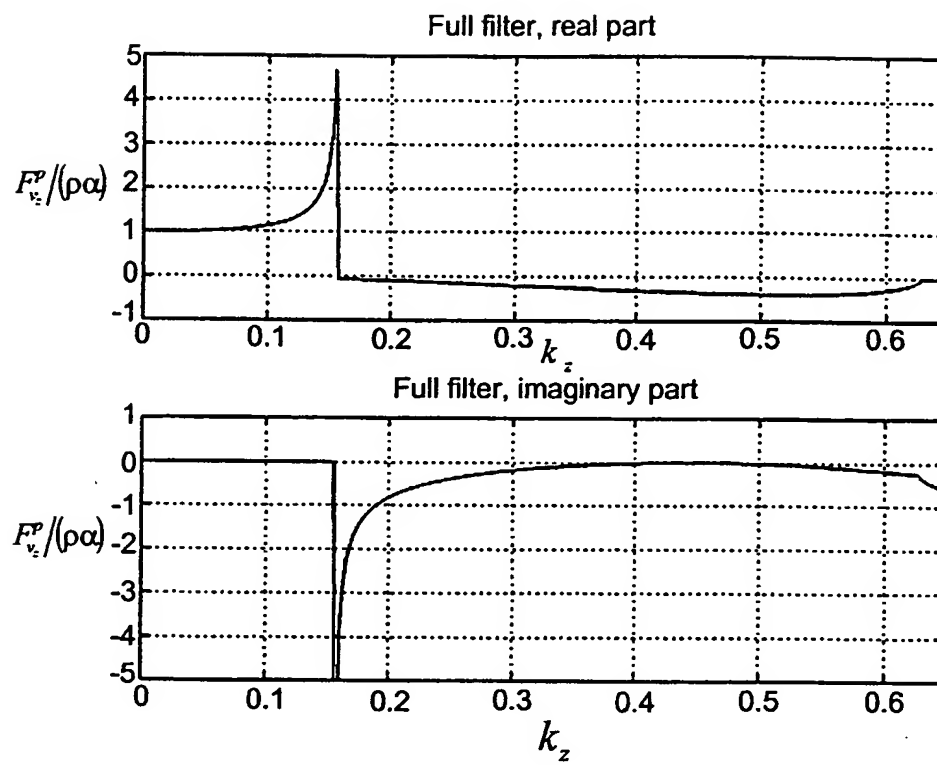


Figure 2 (prior art)

3/13

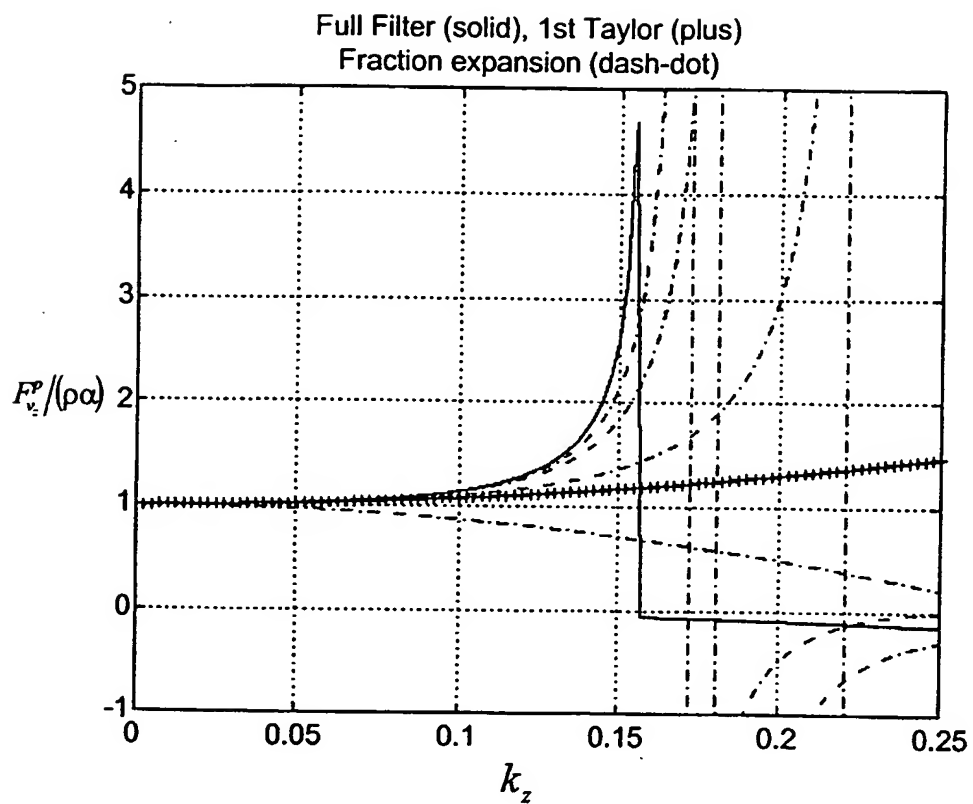


Figure 3 (prior art)

4/13

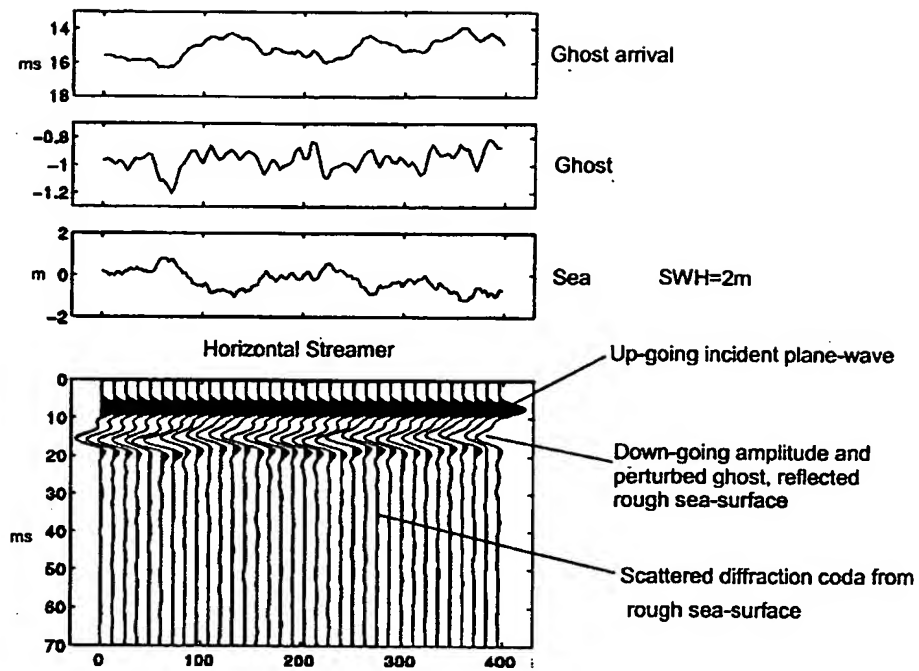


Figure 4

5/13

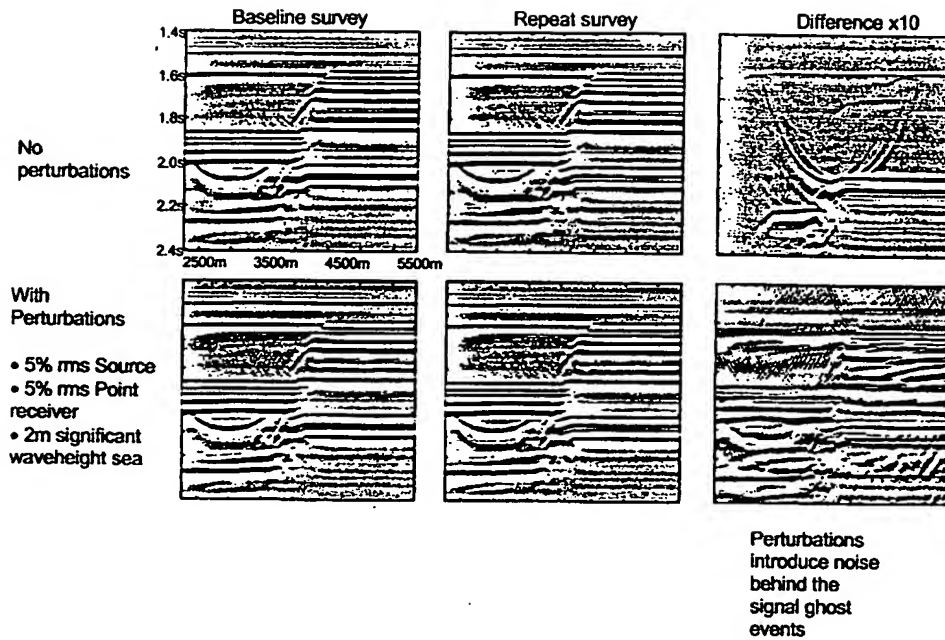
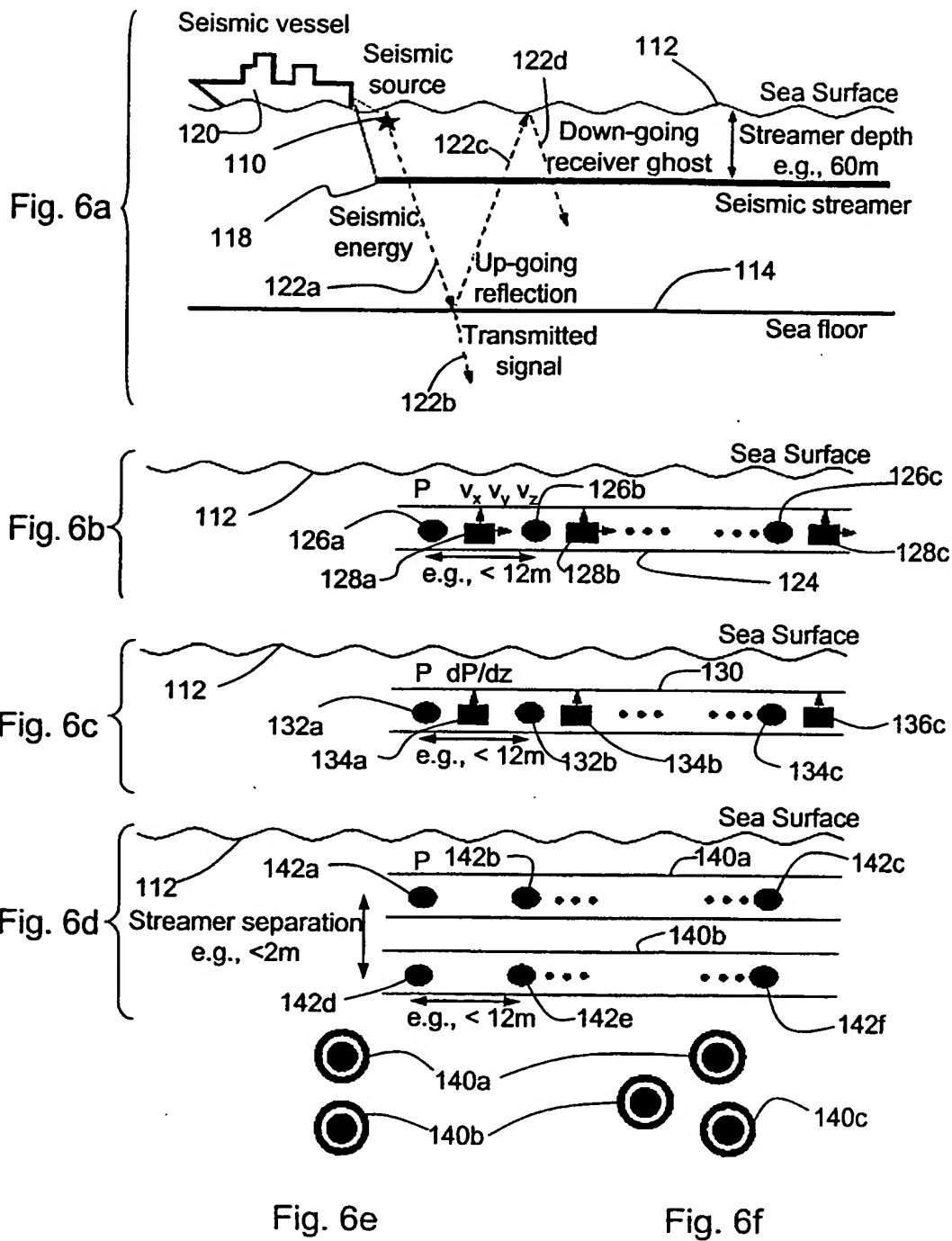


Figure 5

6/13



Figures 6a-f

7/13

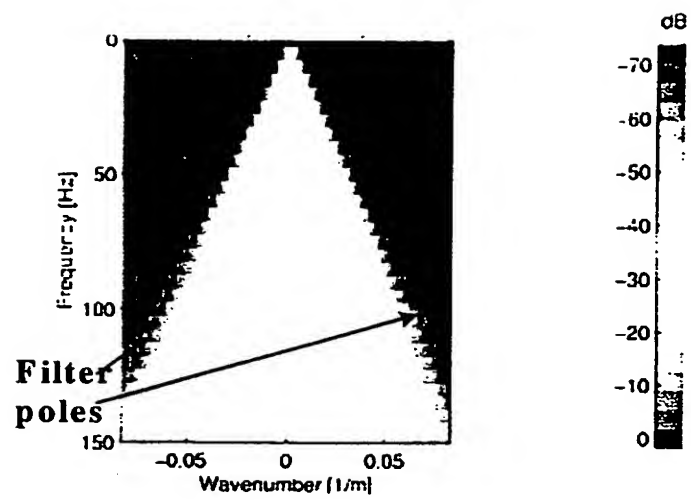


Figure 7

8/13

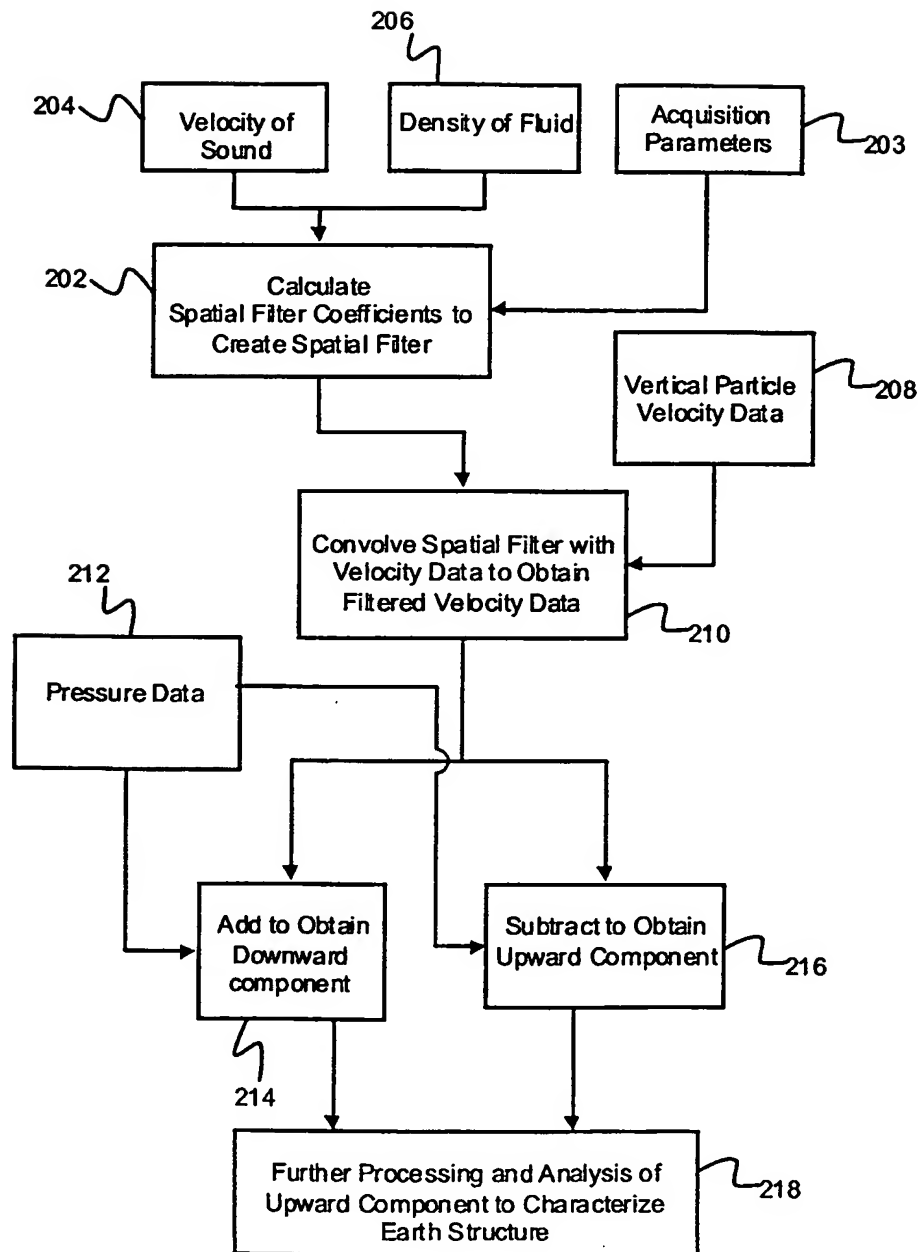


Figure 8

9/13

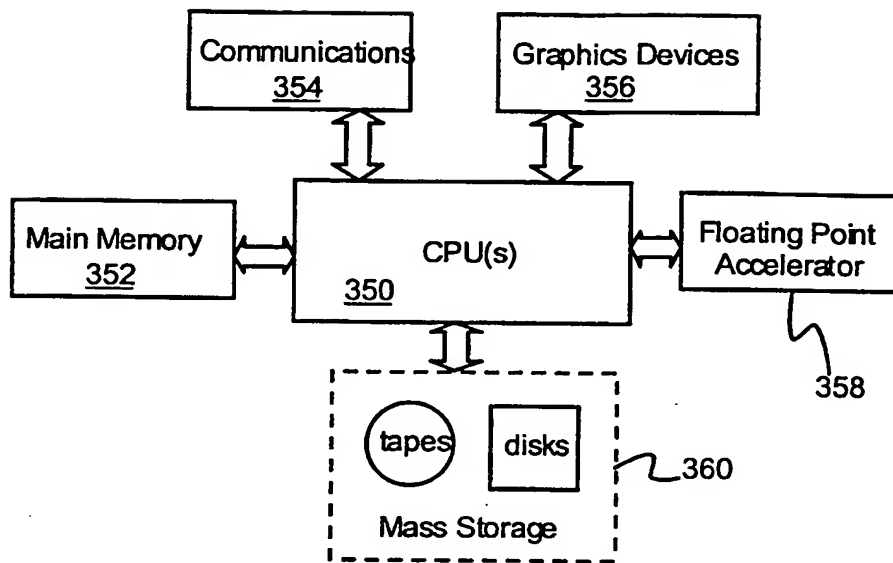


Figure 9

10/13

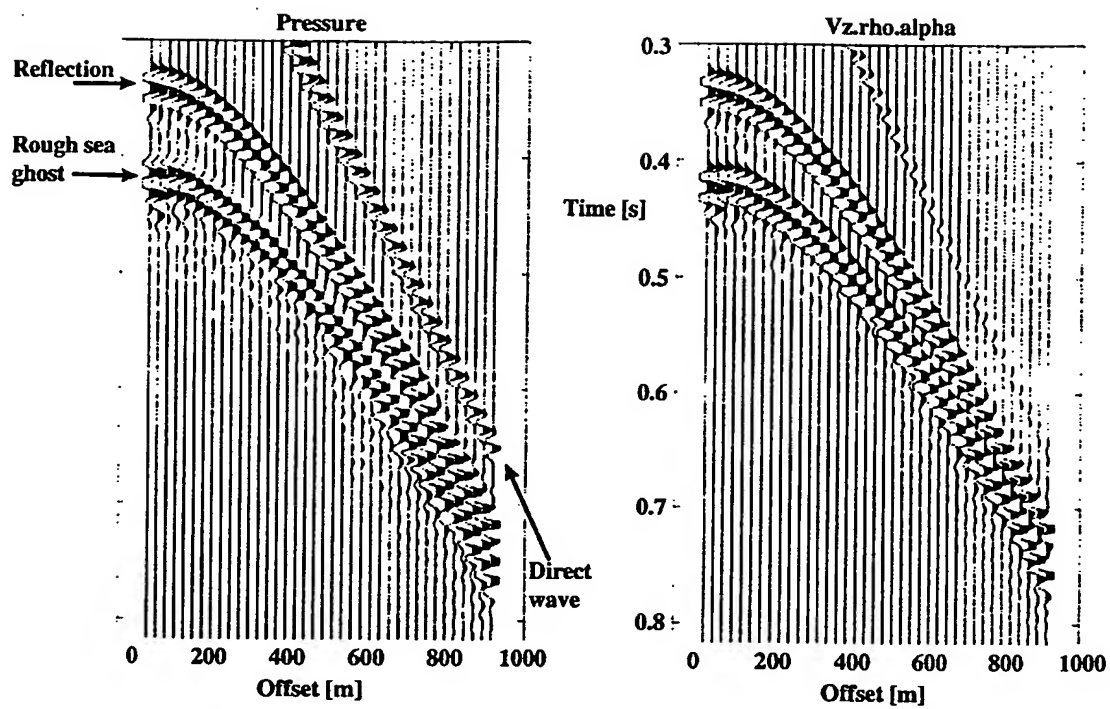


Figure 10

11/13

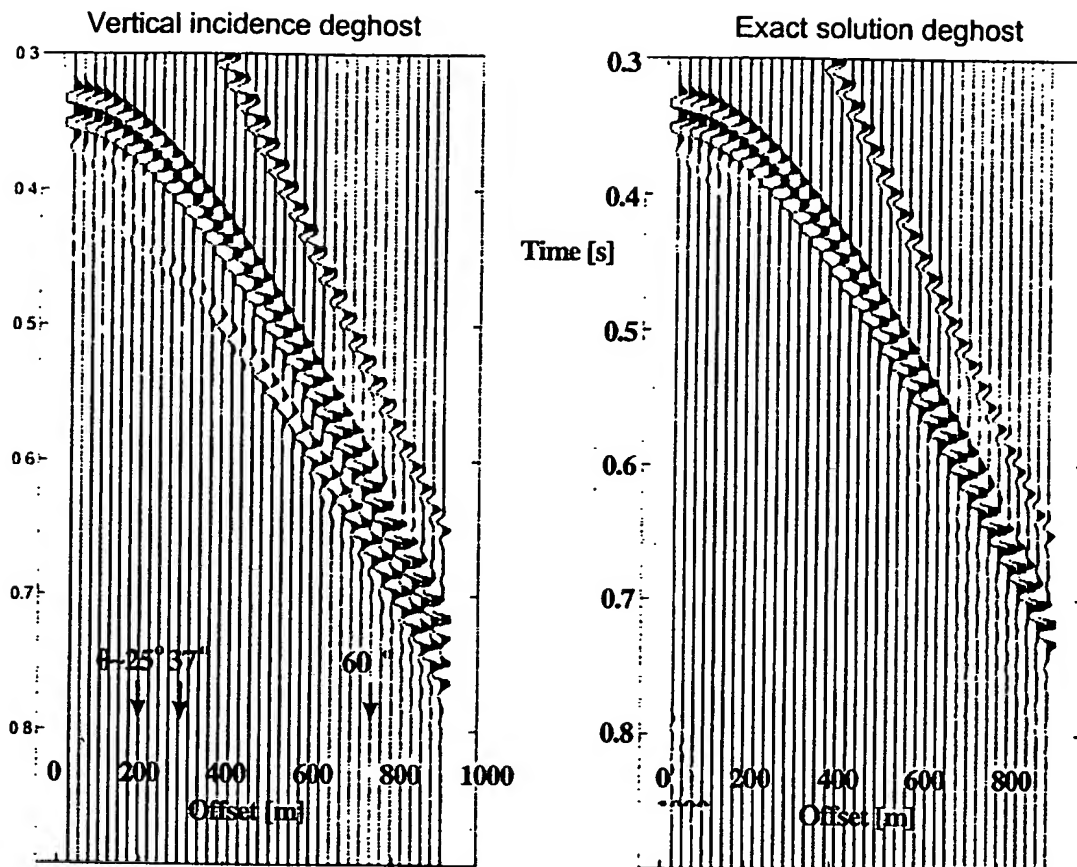


Figure 11

12/13

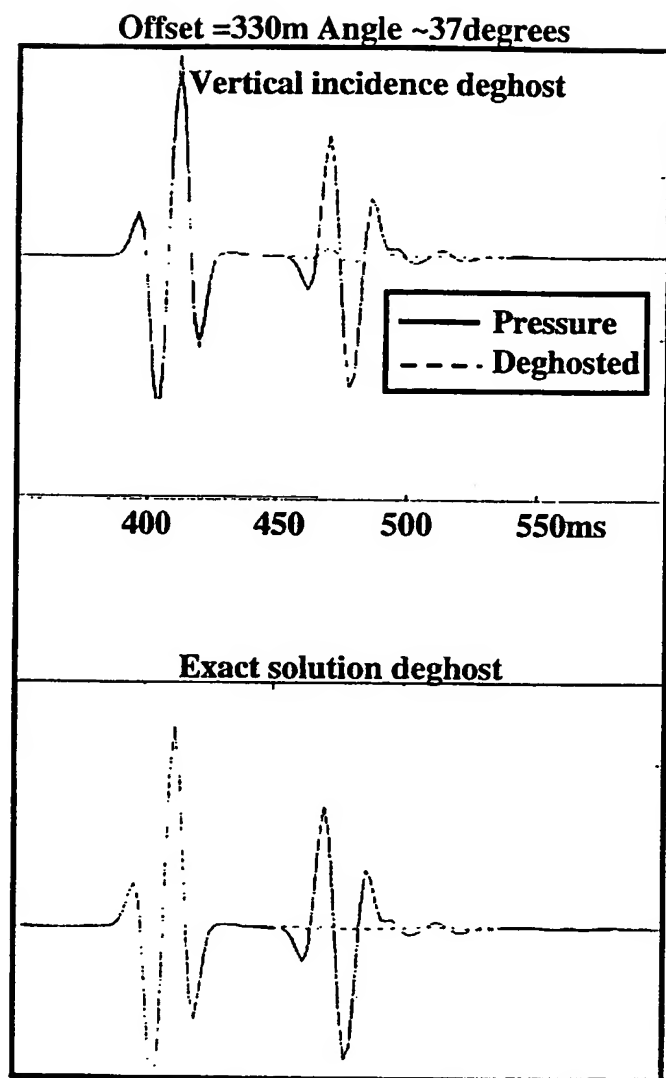


Figure 12

13/13

4C recording

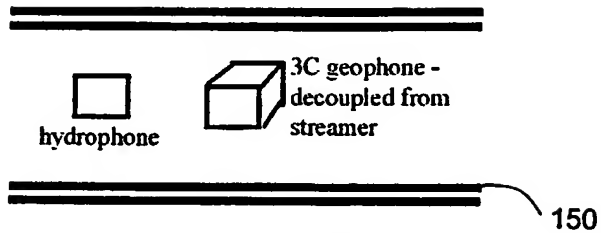


Figure 12a

7C recording

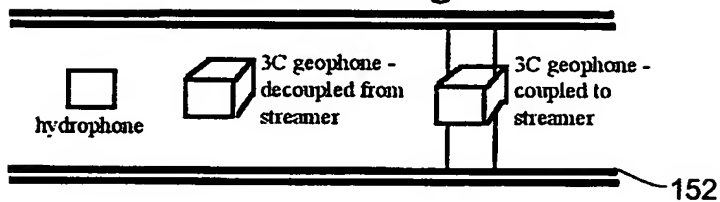


Figure 12b

INTERNATIONAL SEARCH REPORT

International Application No

PCT/GB 00/01074

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 G01V1/36 G01V1/38

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 G01V

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

WPI Data, PAJ, INSPEC, COMPENDEX

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 486 865 A (RUEHLE WILLIAM H) 4 December 1984 (1984-12-04) abstract; claim 1	1,12,18
P,X	GB 2 333 364 A (GECO AS) 21 July 1999 (1999-07-21) cited in the application	1,12,18
Y	abstract page 5, line 10 -page 6, line 5; figure 4	9,13,19
Y	US 3 747 055 A (GREENE E) 17 July 1973 (1973-07-17) column 1, line 54 -column 2, line 14 column 2, line 54 - line 62 column 8, line 25 -column 9, line 8 abstract; figures 1-6	9,13,19
	-/-	

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

30 June 2000

Date of mailing of the international search report

07/07/2000

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040. Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

De Bekker, R

INTERNATIONAL SEARCH REPORT

International Application No

PCT/GB 00/01074

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>BARR F J ET AL: "ATTENUATION OF WATER-COLUMN REVERBERATIONS USING PRESSURE AND VELOCITY DETECTORS IN A WATER-BOTTOM CABLE"</p> <p>ANNUAL MEETING OF SOCIETY EXPL. GEOPHYS. EXPANDED ABSTRACTS, XX, XX, 1 January 1989 (1989-01-01), pages 653-656, XP00G672198</p> <p>the whole document</p> <p>figures 1-3</p>	1,12,18
A	<p>US 4 979 150 A (BARR FREDERICK J)</p> <p>18 December 1990 (1990-12-18)</p> <p>cited in the application</p> <p>abstract; figures 1-9, 14</p> <p>column 1, line 41 -column 2, line 31</p> <p>column 2, line 57 -column 3, line 34</p>	1,12,18
A	<p>AMUNDSEN L ET AL: "EXTRACTION OF THE NORMAL COMPONENT OF THE PARTICLE VELOCITY FROM MARINE PRESSURE DATA"</p> <p>GEOPHYSICS, US, SOCIETY OF EXPLORATION GEOPHYSICISTS, TULSA, vol. 60, no. 1, 1 January 1995 (1995-01-01), pages 212-222, XP000507558</p> <p>ISSN: 0016-8033</p> <p>abstract; figure 1</p> <p>** formula 20 **</p>	1,2,12,18
A	<p>GB 2 090 407 A (MOBIL OIL CORP)</p> <p>7 July 1982 (1982-07-07)</p> <p>abstract; figures 1-5</p> <p>page 1, left-hand column, line 63</p> <p>-right-hand column, line 1</p>	1,12,18
A	<p>US 2 757 356 A (HAGGERTY P.E.)</p> <p>31 July 1956 (1956-07-31)</p> <p>figures 1-7</p>	3-7,14-17,20-23
A	<p>US 4 222 266 A (THEODOULOU SAMUEL M)</p> <p>16 September 1980 (1980-09-16)</p> <p>abstract</p>	7,8
	-/--	

INTERNATIONAL SEARCH REPORT

International Application No

PCT/GB 00/01074

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	SCHNEIDER W A ET AL: "A new data-processing technique for the elimination of ghost arrivals on reflection seismograms" GEOPHYSICS,US,SOCIETY OF EXPLORATION GEOPHYSICISTS. TULSA, vol. 29, no. 5, 1 October 1964 (1964-10-01), pages 783-805, XP002087819 ISSN: 0016-8033 figures 2,3 ----	18
X	US 5 850 622 A (VASSILIOU ANTHONY A ET AL) 15 December 1998 (1998-12-15) figure 7 -----	24-29

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/GB 00/01074

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 4486865 A	04-12-1984	BR 8105589 A CA 1157139 A DE 3134325 A FR 2489530 A GB 2083221 A, B SG 78384 G AU 542118 B AU 7407081 A JP 57074676 A	18-05-1982 15-11-1983 06-05-1982 05-03-1982 17-03-1982 26-04-1985 07-02-1985 11-03-1982 10-05-1982
GB 2333364 A	21-07-1999	FR 2773618 A NO 990153 A	16-07-1999 16-07-1999
US 3747055 A	17-07-1973	NONE	
US 4979150 A	18-12-1990	AU 5716490 A CA 2019007 A, C DE 69018161 D DE 69018161 T EG 19158 A EP 0414344 A NO 303033 B	28-02-1991 25-02-1991 04-05-1995 07-09-1995 29-02-1996 27-02-1991 18-05-1998
GB 2090407 A	07-07-1982	US 4380059 A CA 1254297 A DE 3149525 A NO 813463 A, B,	12-04-1983 16-05-1989 08-07-1982 30-06-1982
US 2757356 A	31-07-1956	NONE	
US 4222266 A	16-09-1980	CA 1136255 A GB 2029582 A, B	23-11-1982 19-03-1980
US 5850622 A	15-12-1998	CA 2242757 A EP 0873527 A NO 983130 A WO 9820367 A	14-05-1998 28-10-1998 07-09-1998 14-05-1998